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A Re-Parameterization Approach for the Construction of domes with planar facets

Romain Mesnil

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A RE- PARAMETERIZATION APPROACH FOR THE CONSTRUCTION OF DOMES WITH PLANAR FACETS

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ABSTRACT

The aim of this article is to propose parameterization with planar facets of dome structures. The technique introduced in this paper starts from an input parameterization and creates a dual pattern with planar quadrilateral facets. The derivation of the analytical solution allows to link the method with the creation of meshes with planar hexagonal facets and of circle packing on spheres. The method can be used in various contexts and allows designers to design with two superimposed parameterizations, which allows for a potential decoupling between structure and envelope.

Keywords: Structural Morphology, Constructive geometry, Fabrication-aware design, PQ-Mesh, gridshell

1. INTRODUCTION

Free-form structures are characterized by an interrelation between mechanical behavior, fabrication process and material. The purpose of structural morphology is to study these relations between different fields. Along the centuries, the importance of shape parameterization in architecture has been demonstrated. For example, the French mathematician Gaspard Monge proposed to cut blocks along the lines of curvature of surfaces, because the normal surface along them is developable and thus simpler to construct [16]. Recent developments in ‘fabrication-aware design’ follow the path of the ‘founder of constructive geometry’, and advocate to use specific parameterizations of surfaces to ease their fabrication. This was the case of Jörg Schlaich, Hans Schober and their team who came up with surfaces of translation and later scale-trans surfaces to construct steel glazed gridshells covered with planar facets [17]. Later, Liu et al. recalled the interest of lines of curvature for this purpose [8]. The problem of covering free-form structures with planar facets is of practical importance, numerous contributions aim at proposing efficient ways to generate so-called conjugate parameterizations of complex shapes [12].

Parameterization is also key to the understanding of numerous optimization problems in structural

mechanics. For example, the solution to the famous Michell truss problem is the construction of an orthogonal parameterization known as Hencky-Prandtl net [19].

Some engineers succeed in merging construction, aesthetics and structural efficiency. Hans Schober and Jörg Schlaich succeeded in constructing ‘transparent shells’, both lightweight and constructible [18]. Chris Williams helped structural engineers Buro Happold and architects Foster+Partners to define the geometry of the gridshell covering the great court of the British Museum with the dynamic relaxation method. The underlying principles used for the parameterization are detailed in [23]. These recent realizations of gridshells tend to merge structure and envelope because of the transparency of glass.

The aim of this paper is to study the well-known question of quadrilateral mesh planarization, while considering two superimposed patterns. Namely, we investigate the possibility to construct a planar quadrilateral mesh that is dual to a given parameterization of a surface. This allows to use one pattern as a structural pattern and the other as an envelope pattern. We put emphasis on patterns derived from principal curvature parameterization and principal stress directions, which are now well-known in the literature on free-form architecture.

We show how to construct a diagonal parameterization on surfaces with positive Gaussian curvature. The practical implications of using the constructed parameterization is discussed with several examples: surfaces of revolution, sphere, moulding surfaces, etc.

The second section recalls properties of conjugate networks and proposes the construction of a conjugate parameterization dual to a reference parameterization. The properties of the constructed parameterization and its relation to remarkable surface discretization are discussed in section 3. Some possible application are shown in the fourth section.

2. GEOMETRY OF PLANAR NETWORKS

We start the discussion by recalling some notions of differential geometry and find the theoretical solution for the problem of surface re-parameterization for planar quadrilateral facets.

2.1. Preliminary statements

In the followings, we consider a surface which is parameterized by its lines of curvatures.

$$\mathbf{f}(u, v) = \begin{pmatrix} x(u, v) \\ y(u, v) \\ z(u, v) \end{pmatrix} \quad (1)$$

In which u and v are parameters and \mathbf{f} is a position vector.

Several notations coexist in the literature on differential geometry, as discussed by Chris Williams in [23], who sets preference on tensor calculus in his theoretical discussion on structural parameterization of surfaces. Tensor calculus allows for concise descriptions of the variations of the different quantities related to surfaces. Green and Zerna used such notations in their reference book on elasticity [5]. Although powerful, this notation is not common for structural engineers, and since this paper does not propose a structural assessment of created patterns, we chose simple notations that do not cover shell theory, similarly to Struik [19]. A letter in subscript indicate partial derivation: for example $\mathbf{f}_u = \frac{\partial \mathbf{f}}{\partial u}$

Lines of curvatures are perpendicular, so that:

$$\mathbf{f}_u \cdot \mathbf{f}_v = 0 \quad (2)$$

Moreover,

$$\mathbf{f}_{uv} \cdot \mathbf{n} = 0 \quad (3)$$

2.2. Construction of a dual planar parameterization

Planar quadrilateral meshes are discrete objects derived from conjugate curve networks. They are defined by a non-linear differential equation [21]:

$$\det(\mathbf{f}_X, \mathbf{f}_Y, \mathbf{f}_{XY}) = 0 \quad (4)$$

Or, more simply put, a parameterization (X, Y) is a conjugate parameterization if the second cross-derivative is in the osculating plane of the surface

$$\mathbf{f}_{XY} \cdot \mathbf{n} = 0 \quad (5)$$

We aim here at constructing such a parameterization, which is locally symmetrical with respect to the curvature line parameterization. It is represented in *Figure 1* and described by equation (6). The name ‘duality’ has many interpretations, and it is not used in the mathematical sense. The idea of creating a conjugate parameterization that is ‘dual’ to another parameterization can be found [3], where the parameterization by the lines of curvatures is dual to a Tchebycheff nets, which allows for the covering of elastic gridshells by planar facets.

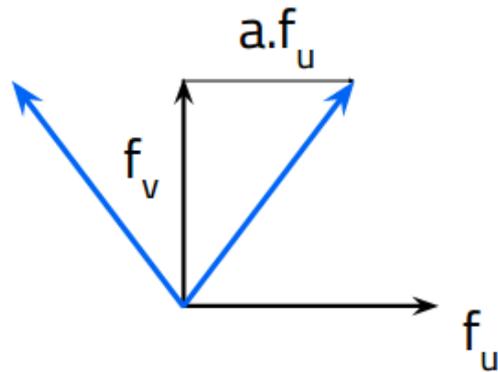


Figure 1: Diagonal parameterization constructed from an initial parameterization

$$\begin{cases} \mathbf{f}_X = u_X \mathbf{f}_u + v_X \mathbf{f}_v \\ \mathbf{f}_Y = u_Y \mathbf{f}_u + v_Y \mathbf{f}_v \\ \frac{u_X}{v_X} = -\frac{u_Y}{v_Y} = a(u, v) \end{cases} \quad (6)$$

The cross derivative is simply computed as follows:

$$\mathbf{f}_{XY} = u_{XY}\mathbf{f}_u + u_X u_Y \mathbf{f}_{uu} + (u_X v_Y + u_Y v_X)\mathbf{f}_{uv} + v_{XY}\mathbf{f}_v + v_X v_Y \mathbf{f}_{vv} \quad (7)$$

We can thus evaluate the component along the normal of the surface \mathbf{n} , defined as $\mathbf{n} = \mathbf{f}_u \wedge \mathbf{f}_v$.

$$\mathbf{f}_{XY} \cdot \mathbf{n} = u_X u_Y \mathbf{f}_{uu} \cdot \mathbf{n} + (u_X v_Y + u_Y v_X)\mathbf{f}_{uv} \cdot \mathbf{n} + v_X v_Y \mathbf{f}_{vv} \cdot \mathbf{n} \quad (8)$$

This expression can be simplified when (u,v) is a curvature line parameterization and satisfies equation (3):

$$\mathbf{f}_{XY} \cdot \mathbf{n} = u_X u_Y \mathbf{f}_{uu} \cdot \mathbf{n} + v_X v_Y \mathbf{f}_{vv} \cdot \mathbf{n} \quad (9)$$

Since we are looking for conjugate parameterizations, this quantity must satisfy equation (5). This imposes a restriction on the value of a :

$$-a^2 \mathbf{f}_{uu} \cdot \mathbf{n} + \mathbf{f}_{vv} \cdot \mathbf{n} = 0 \quad (10)$$

Assuming that (u,v) is a curvature line parameterization, we can express the quantities $\mathbf{f}_{uu} \cdot \mathbf{n}$ and $\mathbf{f}_{vv} \cdot \mathbf{n}$ with the principal curvatures κ_u and κ_v . First, we notice that equation (10) is well posed only if the surface has positive Gaussian curvature. It follows that

$$a = \frac{\|\mathbf{f}_v\|}{\|\mathbf{f}_u\|} \sqrt{\frac{\kappa_v}{\kappa_u}} \quad (11)$$

3. DISCUSSION

3.1. Link with Dupin's indicatrix and planar hexagonal meshes

Wang *et al.* showed that vertices of a hexagonal mesh with planar facets converge towards Dupin indicatrix of the underlying surface [25]. Our result

shows a remarkable relation with this construction, which is illustrated in *Figure 2*.

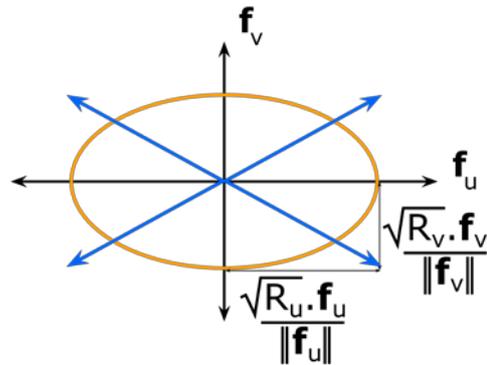


Figure 2: Dupin indicatrix as an ellipse: principal curvature direction (black) and the parameterization constructed in this paper (blue)

Indeed, in positive curvature area, Dupin's indicatrix is an ellipse, and the ratio of the semi-axes lengths is:

$$\frac{l_u}{l_v} = \frac{\sqrt{R_u}}{\sqrt{R_v}}$$

In the (u,v) coordinates, one must take into account that \mathbf{f}_u and \mathbf{f}_v are not unitary. This is equal to the ratio a computed previously in equation (11).

In planar hexagonal meshes, one is able to naturally extract three families of developable strips, which are highlighted in *Figure 3*. One family of strips is aligned with a principal curvature direction, while the two others are aligned with the parameterization constructed in this article. Regular planar hexagonal meshes are notably difficult to obtain because one must control the metric of the parameterization.

Our considered parameterization cannot be constructed for surfaces with negative Gaussian curvature. It should be noticed that for surfaces of negative Gaussian curvature, the Dupin's indicatrix is a hyperbola, so that the resulting strips are not smooth.

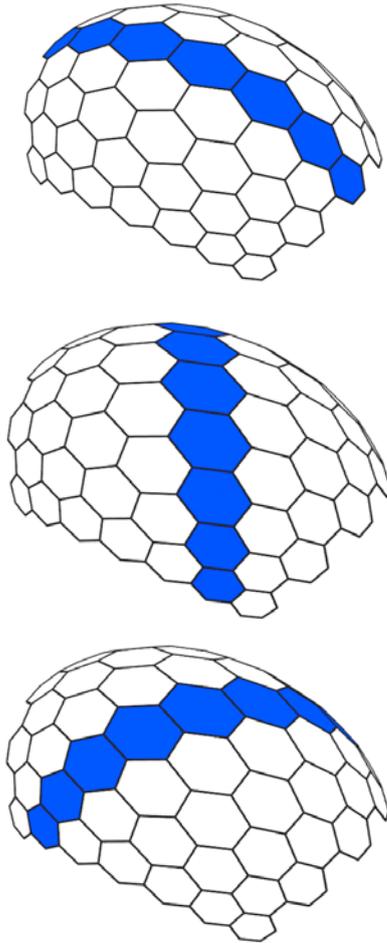


Figure 3: A hexagonal mesh with planar facets: alignment of the mesh with principal curvature (top) and the dual parameterization constructed in this paper (center and bottom)

Finally, it can be noticed that the parameterization constructed in equation (11) corresponds to the imaginary asymptotes of the ellipse [22]. It is interesting to recall that the asymptotic directions in surfaces with negative Gaussian curvature are self-conjugated: and cannot be used to construct quadrilateral meshes with planar facets [8]. A fundamental difference between surfaces of positive or negative curvature is thus illustrated by our construction.

3.2. Surfaces of revolution

The lines of curvature of surfaces of revolution are the meridians and parallels. They are therefore extremely simple to characterize from an analytical point of view and we propose here to study the properties of the diagonal parameterization constructed in this paper.

$$\cos \alpha = \sqrt{\frac{\kappa_v}{\kappa_u}} \tag{12}$$

The curvatures κ_u and κ_v remain constant along parallels, the angle of the parameterization is thus also constant. This guarantees already good repetition of elements in the constructed parameterization. We propose to find surfaces so that the angle does not vary along the parallels either. Such parameterizations are known as loxodromic parameterizations: the loxodromic, also called rhumb lines, make a constant angle with the meridians.

We consider a surface of revolution with following cylindrical equation:

$$\begin{cases} x(t, \varphi) = \rho(t) \cos \varphi \\ y(t, \varphi) = \rho(t) \sin \varphi \\ z(t, \varphi) = h(t) \end{cases}$$

In the followings, we assume that $\rho_t^2 + h_t^2 = 1$ and compute the couple (ρ, h) so that $\sqrt{\frac{\kappa_\varphi}{\kappa_t}} = \beta$. The computation of the principal curvatures is classical [7] and yields a couple of nonlinear equations.

$$\begin{cases} \rho \cdot \rho_{tt} + \beta(1 - \rho_t^2) = 0 \\ \rho_t^2 + h_t^2 = 1 \end{cases} \tag{13}$$

The first equation in (13) depends on ρ only. Its solution is not expressed with classical functions for general values of β . We shall notice however that there is an obvious solution for $\beta = 1$:

$$\begin{cases} \rho = \cos t \\ h = \sin t \end{cases} \tag{14}$$

We find thus the well-known parameterization of the sphere. In the case of a sphere, the principal curvatures are indeed a constant and $\cos \alpha = 1$, so that the two networks of the diagonal parameterization make a constant angle of 90° . This theoretical solution has been applied on a notable example: the Maritime Museum of Osaka designed by Paul Andreu, Tohata Architects and Ove Arup & Partners. We shall notice however that the designers constructed the pattern with another rule and were not certain that the spiraling curves were loxodromic curves [6].



Figure 4: Osaka Maritime Museum: a spiraling pattern following loxodromic curves and creating a PQ-Mesh

Other values of β can be used, yielding different shapes. The numerical solution of equation (13) is found with the integration of a finite difference scheme detailed in the appendix. Some profile curves are represented in **Figure 5**. Large values of β correspond to high rise-over-span ratio whereas small values of β result in shallow profile curves.

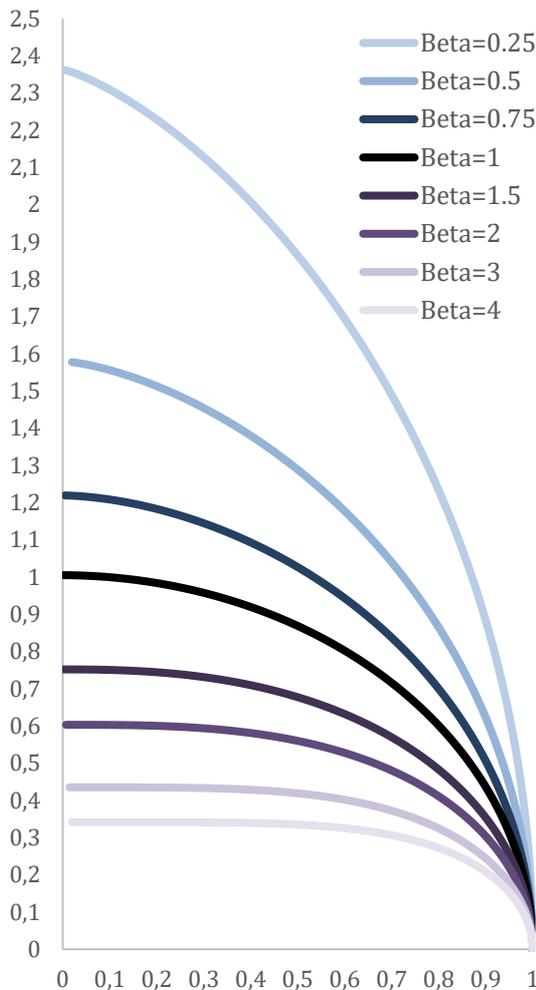


Figure 5: Profile curve of surfaces of revolution where loxodromic curves create a conjugate curve network

3.3. Sphere meshing

We consider now patterns derived from lines of curvature on spheres. Equation (11) can be simplified in the case of a sphere:

$$\begin{cases} f_X = \|f_v\| \cdot f_u + \|f_u\| \cdot f_v \\ f_Y = -\|f_v\| \cdot f_u + \|f_u\| \cdot f_v \end{cases}$$

This can be written as follows:

$$\begin{cases} f_X = f_U + f_V \\ f_Y = -f_U + f_V \end{cases}$$

with

$$\begin{cases} f_U = \|f_v\| \cdot f_u \\ f_V = \|f_u\| \cdot f_v \end{cases} \quad (15)$$

The parameterization (U,V) is isothermic because it satisfies two identities:

$$\begin{cases} \|f_U\| = \|f_V\| \\ f_U \cdot f_V = 0 \end{cases}$$

This construction admits a discrete counterpart, already discussed by Bobenko and Springborn [2]. Isothermic parameterizations of the sphere can indeed be constructed from circle packings. The top of **Figure 6** shows a circle packing on a sphere: connected circles touching tangentially at one point. A mesh can be constructed so that the circles are in-circles of the facets: it corresponds to a discrete isothermic parameterization of the sphere. Another circle packing, dual to the first one can be constructed so that the circles of the two circle packing are perpendicular and share the same contact points between circles. This second circle packing is shown in light orange in **Figure 6**. From the two circle packing, one can create a circular mesh, with the vertices of all facets inscribed in a circle.

This remark further demonstrates that the dual parameterization introduced in this article is constrained in practice. For a given pattern connectivity, the circle packing is indeed unique up to a Möbius transformation.

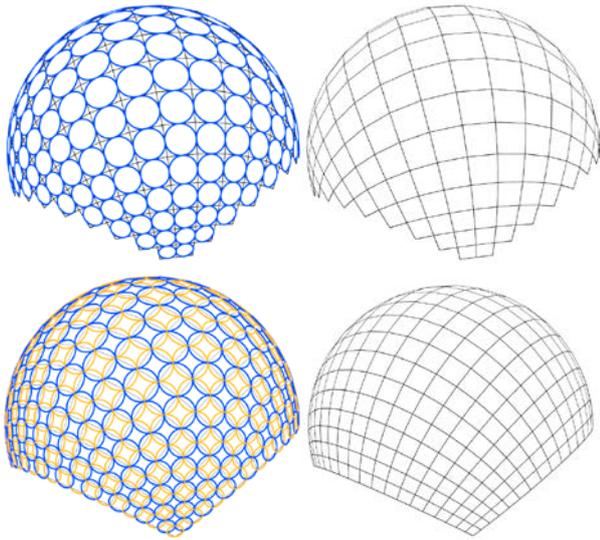


Figure 6: Circle packing on a sphere: isothermic parameterization (top) and corresponding dual parameterization derived in this article (bottom)

4. APPLICATIONS

4.1. Implementation

The examples presented in the present paper are computed on NURBS surfaces, where the computation of the derivatives is exact and fast. We use the classical Runge-Kutta method for the vector field integration.

It is also possible to perform vector field integration on meshes with methods already existing in the literature [9].

4.2. Gridshells with high node congruence

High node repetition can be obtained by applying parallel transformations to meshes with node congruence, because such transformations leave the geometry of nodes invariant. This principle has been applied to the networks of lines of curvature in [10]. It can be extended to the loxodromic parameterization of surfaces of revolutions proposed in this paper.

4.3. Pattern superposition

The parameterization proposed in this article offers the potential to work with two different patterns for the structure and envelope. The curve network following the parameterization satisfying equation (10) have their intersection at constant values of u and v . Consider **Figure 7**: the blue lines represent

the conjugate parameterization constructed from equation (9) while the black dotted lines represent isocurves of the initial parameterization. The blue lines intersect along the iso-curves (solid circles): the white circles indicates that only a subset of the isocurve network is used.

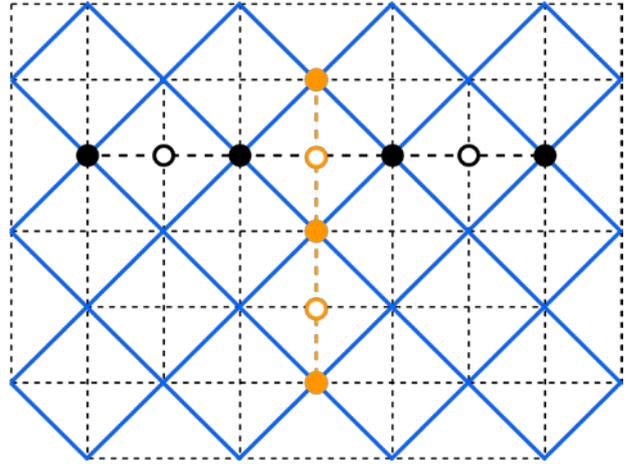


Figure 7: Two superposed parameterization: the vertices of the blue and black dashed patterns are in common

The literature on free-form structures does not offer many examples of pattern superposition strategies, one of the only ones being the gridshells of the Paunsdorf Center, which uses a triangular structural pattern and a quadrangular pattern for glazing, as shown in **Figure 8** [18]. Triangular gridshells are known to be significantly stiffer than quadrangular gridshells, and quadrangles have better nesting properties than triangles, so this solution uses the advantages of both solutions.

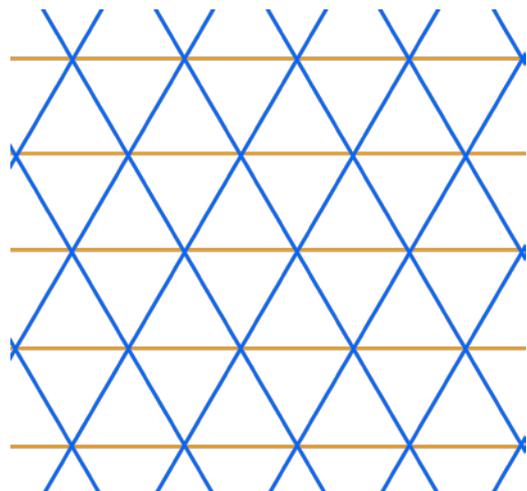


Figure 8: Patterns used for the Paunsdorf gridshell: the glazing pattern (blue) and structural pattern (orange and blue)

Our approach allows to use different strategies for patterning, for example if the structural pattern follows structurally optimal load paths. It can also be extended to other patterning strategies, like the Kagome pattern. Indeed, Kagome gridshells have better performance than quadrangular patterns, with the same node valency [13][14]. The nesting of triangles and hexagons is however not as efficient as the nesting of quadrilaterals, so exploring the same idea as the one developed for the Paunsdorf Center gridshell is a possibility offered by our approach.

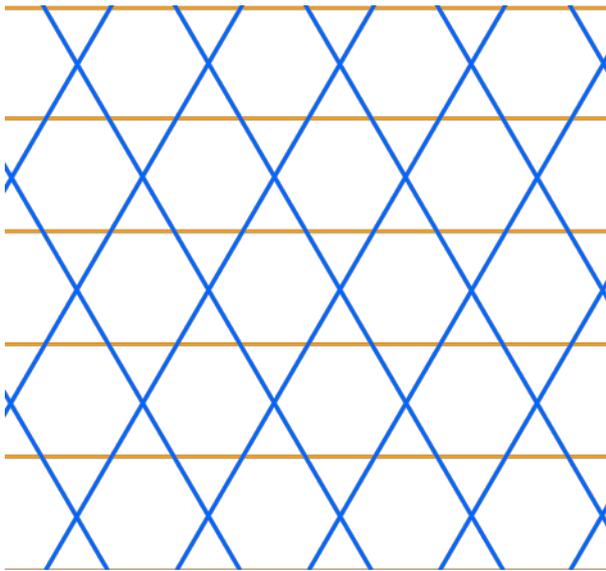


Figure 9: A kagome grid pattern: envelope (blue) and structure (blue and orange)

Notice however that the pattern superposition imposes strong constraints on the metric because of equation (10). This is obvious with the sphere, where the initial pattern must derive from an isothermic parameterization. The designer loses thus degrees of freedom on the subdivision of the initial mesh.

4.4. Structurally optimal patterns

Structurally optimal pattern in plates are known to follow lines of principal stress. When a load case is dominant, it is meaningful to take inspiration from the principal stress orientation to derive a structural pattern, as illustrated by ribbed slabs designed by Pier Luigi Nervi [1]. This approach is however difficult to generalize to lightweight structures, where the self-weight is not the governing load for the structural design.

Remarkably, lines of curvature are also lines of principal stress for uniform normal load for a family of surfaces, for example isothermic surfaces [15]. Isothermic surfaces cover a large range of shapes, like minimal surfaces, constant mean-curvature surfaces, quadrics, like the ellipsoid. Gaspard Monge illustrated the potential of his findings by proposing the design of a vault with the blocks aligned with the principal curvatures of an ellipsoid. This was a computational tour de force at that time, and the result was highly aesthetical. We propose to re-investigate the patterning of ellipsoids with the method proposed in this article. The result can be seen in *Figure 10* and *Figure 11*.

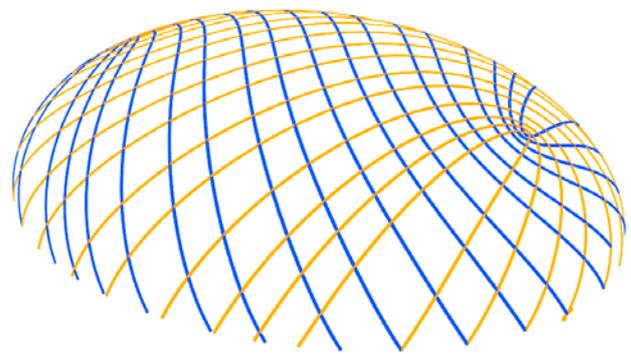


Figure 10: Conjugate curve network on an ellipsoid constructed with our method

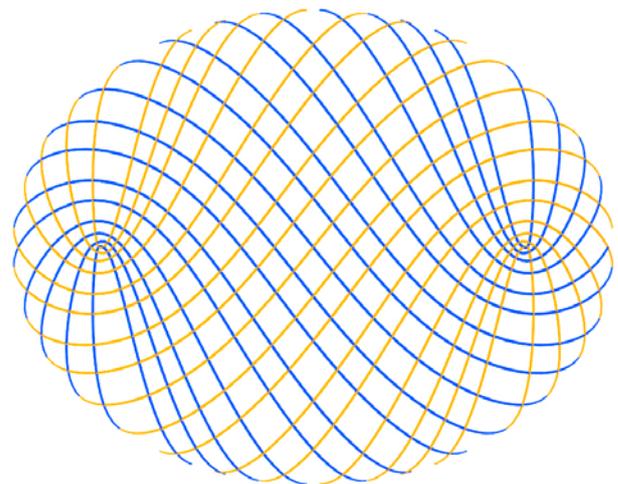


Figure 11: Conjugate curve network dual to the lines of curvature on an ellipsoid

The pattern superposition approach offers thus a potential for the creation of efficient structures with elegant parameterizations.

4.5. PQ-meshes and developable strips

Figure 12 shows a stadium geometry based on a moulding surface. Moulding surfaces are generated by the sweeping of a planar curve along a planar rail curve. Alternatively, they can be viewed as images of surfaces of revolution by parallel transformations [10]. Their lines of curvature are planar, which simplifies their assembly and construction. Moulding surfaces are regularly used for the geometric generation of stadia.

The pattern showed in **Figure 12** is dual to lines of curvatures. It breaks the reading of these planar curves, and highlights the visual potential of the spiraling patterns arising from our re-parameterization approach. Note that similar looking diagrid patterns have been used in recent stadia projects, like the Arena da Amazônia, built in Manaus, Brazil in 2014[4]. In this project, the diagrid behaves like a gridshell, and is stabilized by a compression ring at the inner edge and by a tension ring at the outer edge. Therefore, the alignment of the pattern with the edges of the surface is a necessary condition to guarantee a proper structural behavior, so that the approach proposed in this article could be used for this purpose.

Finally, the Arena da Amazônia was covered with a PTFE membrane: the method proposed in this article could extend the range of materials or technologies for covering, for example with developable panels which could fulfil a structural purpose as a bracing system. In **Figure 12**, one of the developable surface created by the parameterization is shown in light blue, while a developable surface resulting from the curvature line parameterization is depicted in light orange.

5. CONCLUSION

This article introduced a re-parameterization technique on curved shapes that yields planar quadrilateral facets. The main advantage of the method is that it allows the superposition of a structural pattern and an envelope pattern. The construction of the solution is linked with classical objects of discrete geometry: circle packing on spheres and hexagons.

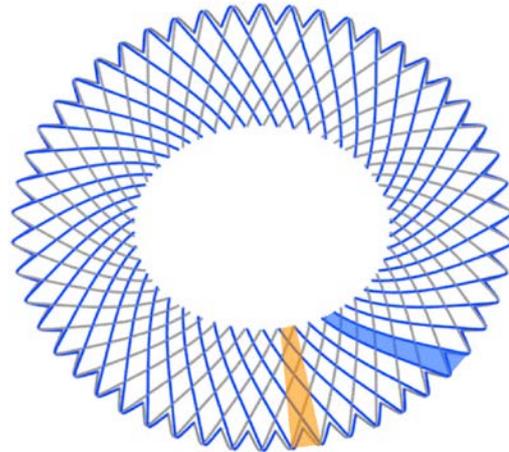
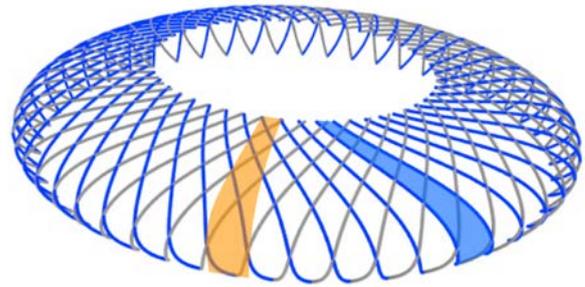


Figure 12: A stadium geometry based on a moulding surface: perspective (top) and plane view (bottom). The surface between two consecutive curves of the same color is developable (shown in blue)

We described the surfaces which admit a conjugate curve parameterization by its rhumb lines with a system of nonlinear equations. The analytical solution has been derived for specific cases, and a discrete integration scheme has been proposed. The resulting structures have a constant angle and planar facets.

The proposed method allows the designer to manipulate and combine two parameterizations. This allows the separation of structural pattern and envelope pattern and should open new possibilities for the structural design of domes.

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PHOTO CREDITS

Figure 4 is licensed under the Creative Commons Attribution 2.5 Generic license. Complementary informations can be found on this link:

https://commons.wikimedia.org/wiki/File:Osaka_maritime_museum01s3200.jpg

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APPENDIX 1: INTEGRATION OF LOXODROMIC

Equation (12) cannot be solved using usual functions. We implement thus a finite difference scheme for its integration. We use the central finite difference,

$$\begin{cases} \rho_{tt}(t) = \frac{\rho(t + \Delta t) - 2 \cdot \rho(t) + \rho(t - \Delta t)}{\Delta t^2} + \mathcal{O}(\Delta t^2) \\ \rho_t(t) = \frac{\rho(t + \Delta t) - \rho(t - \Delta t)}{2\Delta t} + \mathcal{O}(\Delta t^2) \end{cases}$$

We write $\rho(t + \Delta t) = \rho^+$ and $\rho(t - \Delta t) = \rho^-$, so that equation (13) becomes:

$$\rho \cdot \frac{\rho^+ - 2\rho + \rho^-}{\Delta t} + \beta \left(1 - \frac{(\rho^+ - \rho^-)^2}{4\Delta t^2} \right) + \mathcal{O}(\Delta t^2) = 0$$

Assume that one knows ρ^- and ρ : the equation is simply a second order equation in ρ^+ and has an obvious solution. For the initialization, we assume that $\rho_t = 0$, so that $\rho(\Delta t) = \rho(-\Delta t)$. The first step of the algorithm is expressed as follows:

$$\rho \cdot \frac{2\rho^+ - 2\rho}{\Delta t} + \beta + \mathcal{O}(\Delta t^2) = 0$$

So that the solution is

$$\rho^+ \sim \rho - \frac{\beta \Delta t}{2\rho}$$

The finite difference methods allows thus to integrate the value of ρ . The value of h is found by integrating the following equation by using the central difference scheme:

$$h_t = \sqrt{1 - \rho_t^2}$$