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Workgroup on Computational Mechanics of Generalized Continua  
and Applications to Materials with Microstructure

# Stress-gradient materials: an analytical exploration

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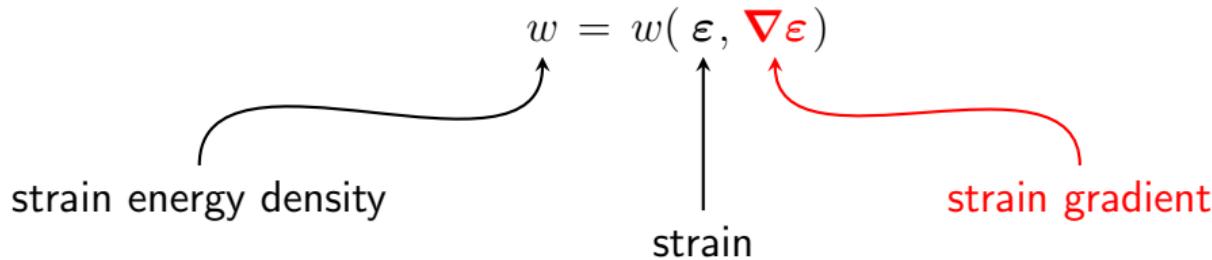
MSME  
Laboratoire Modélisation et Simulation Multi Echelle

École des Ponts  
ParisTech

# Motivation (1)

At first glance...

## Strain gradient elasticity theory



Mindlin, R.D., Eshel, N.N., 4, pp. 109–124, International Journal of Solids and Structures, 1968

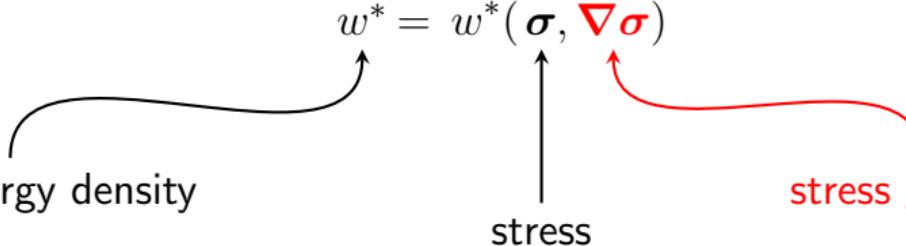
# Motivation (2)

At first glance...

## Strain gradient elasticity theory

$$w = w(\boldsymbol{\varepsilon}, \nabla \boldsymbol{\varepsilon})$$

## Stress gradient elasticity theory

$$w^* = w^*(\boldsymbol{\sigma}, \nabla \boldsymbol{\sigma})$$




# Motivation (3)

At first glance...

## Strain gradient elasticity theory

$$w = w(\boldsymbol{\varepsilon}, \nabla \boldsymbol{\varepsilon})$$

## Stress gradient elasticity theory

$$w^* = w^*(\boldsymbol{\sigma}, \nabla \boldsymbol{\sigma})$$

Is stress gradient elasticity equivalent or complementary to strain gradient elasticity?



# Objective

## Outline

- ? How does stress gradient elasticity theory (Forest and Sab, 2012) differ from strain gradient one?
- Stress gradient elasticity theory (Forest and Sab, 2012).
- Closed form solution to Eshelby spherical inhomogeneity problem.
- Homogenization of heterogeneous stress-gradient materials (Mori Tanaka estimate)

S. Forest, K. Sab Mechanics Research Communications, 40, pp. 16–25, 2012  
K. Sab, F. Legoll, S. Forest accepted for publication, Journal of Elasticity, 2015

# Decomposition of stress gradient tensor

The spherical and deviatoric part of a third order tensor

## Strain gradient tensor

- "free"

## Stress gradient tensor

- constrained

$$\nabla \cdot \sigma + \mathbf{b} = 0 \Leftrightarrow (\nabla \sigma) : \boldsymbol{\delta} + \mathbf{b} = 0$$

## Decomposition of stress gradient tensor

$$\nabla \sigma = \mathbf{J} \therefore \nabla \sigma + \mathbf{K} \therefore \nabla \sigma$$

↑                                   ↑

spherical projector                                   deviatoric projector

$$J_{ijklmn} = \frac{1}{8} (\delta_{ik}\delta_{jl}\delta_{mn} + \delta_{ik}\delta_{jm}\delta_{ln} + \delta_{il}\delta_{jk}\delta_{mn} + \delta_{im}\delta_{jk}\delta_{ln})$$

$$K_{ijklmn} = I_{ijklmn} - J_{ijklmn}$$

## Stress energy density function

$$w^* = w^*(\boldsymbol{\sigma}, \underbrace{\mathbf{K} : : \nabla \boldsymbol{\sigma}}_{\mathbf{R}})$$

For isotropic stress gradient materials:

$$w^*(\boldsymbol{\sigma}, \mathbf{R}) = \frac{1}{2} \boldsymbol{\sigma} : \mathbf{S} : \boldsymbol{\sigma} + \frac{1}{2} \mathbf{R} : : \mathbf{M} : : \mathbf{R}$$

## Constitutive laws

$$\mathbf{e} = \frac{\partial w^*}{\partial \boldsymbol{\sigma}} = \mathbf{S} : \boldsymbol{\sigma}, \quad \Phi = \frac{\partial w^*}{\partial \mathbf{R}} = \mathbf{M} : : \mathbf{R}$$

NOTA:  $\Phi, \mathbf{R}$  have to be deviatoric tensors!

$$\mathbf{M} = \mathbf{K} : : \mathbf{M} : : \mathbf{K}$$

# Simplified stress / strain gradient elasticity

A comparison of field equations (no body force)

	Simplified stress gradient	Simplified strain gradient
Equilibrium	$\sigma_{ij,j} = 0$	$\tau_{ij,j} = 0$
Gradient	$R_{ijk} = \sigma_{ij,k}$	$\kappa_{ijk} = \varepsilon_{ij,k}$
Constitutive laws	$e_{ij} = S_{ijkl}\sigma_{kl}$ $e_{ij} = \varepsilon_{ij} + \Phi_{ijk,k}$ $\Phi_{ijk} = \ell^2 K_{ijkpqr} S_{pqmn} R_{mnr}$	$\sigma_{ij} = C_{ijkl}\varepsilon_{kl}$ $\tau_{ij} = \sigma_{ij} - \mu_{ijk,k}$ $\mu_{ijk} = \ell^2 C_{ijmn} \kappa_{mnk}$
SUBC	$\sigma_{ij} = \Sigma_{ij}$	$\sigma_{ij} n_j - (\mu_{ijk} n_k)_{,j} + (\mu_{ijk} n_k n_l)_{,l} n_j = t_i$ on $\partial\Omega$ (smooth part) $\mu_{ijk} n_j n_k = q_i$ on $\partial\Omega$ (smooth part) $[[\mu_{ijk} m_j n_k]] = 0$ on the edge of $\partial\Omega$

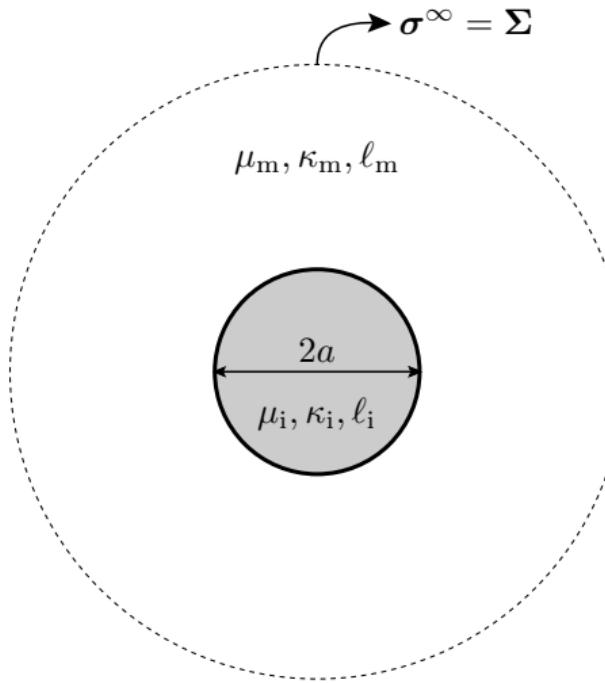
S.Forest, K. Sab Mechanics Research Communications, 40, pp. 16–25, 2012

Altan, B.S., Aifantis, E.C., Journal of the Mechanical Behavior of Materials, 8(3), pp. 231–282, 1997

Gao, X.-L., Park, S.K. International Journal of Solids and Structures, 44, pp. 7486–7499, 2007

# Eshelby's spherical inhomogeneity problem (1)

Geometry + mechanical properties



## Stress gradient (this work):

- Uniform isotropic stress:

$$\Sigma = \mathbf{e}_x \otimes \mathbf{e}_x + \mathbf{e}_y \otimes \mathbf{e}_y + \mathbf{e}_z \otimes \mathbf{e}_z$$

- Uniform axial stress:

$$\Sigma = \mathbf{e}_z \otimes \mathbf{e}_z$$

## Strain gradient:

- Gao, X.-L., Ma, H.M Acta Mechanica, 207 (3), pp. 163-181, 2009
- Gao, X.-L., Ma, H.M Journal of the Mechanics and Physics of Solids, 58 (5), pp. 779-797, 2010

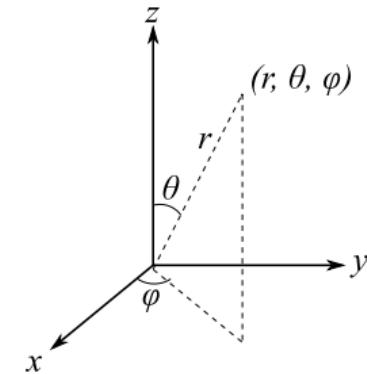
## Postulated stress form in spherical coordinates (similar to Love's approach)

- Uniform isotropic stress prescribed at boundary:

$$\sigma = \sigma(r)$$

- Uniform axial stress prescribed at boundary:

$$\sigma = \sigma(r, \theta)$$



## Continuity conditions at the surface matrix-inclusion

$$\sigma_m(r = a) = \sigma_i(r = a)$$

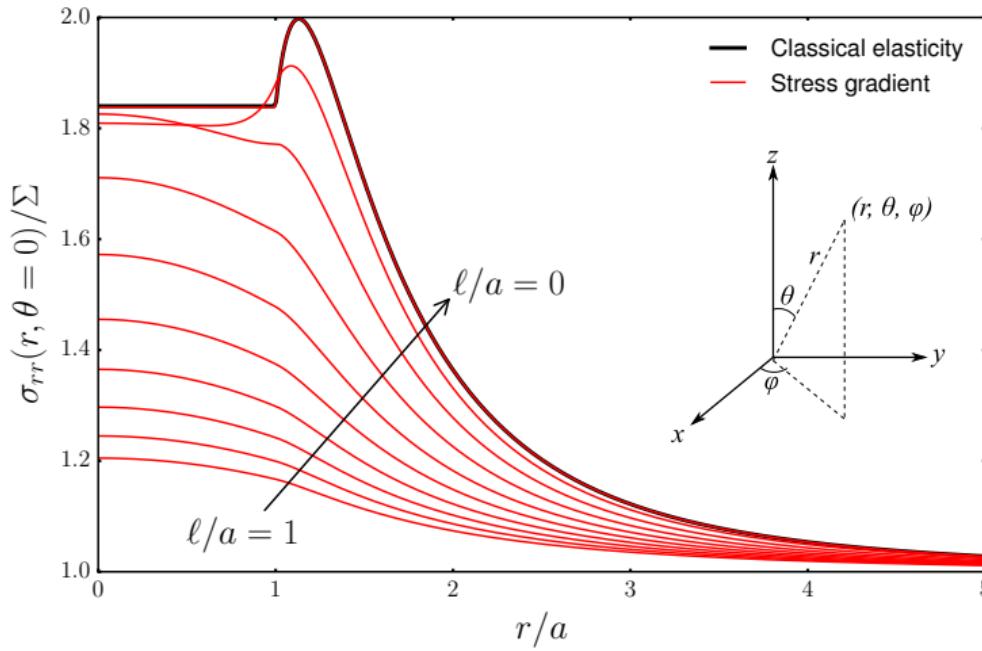
$$[\mathbf{u} \otimes^s \mathbf{n} + \Phi \cdot \mathbf{n}]_m(r = a) = [\mathbf{u} \otimes^s \mathbf{n} + \Phi \cdot \mathbf{n}]_i(r = a)$$

Love, A.E.H. Dover Publications, New York, 1944

# Uniaxial problem $\Sigma = \mathbf{e}_z \otimes \mathbf{e}_z$

Radial stress field  $\sigma_{rr}(r, \theta = 0)$

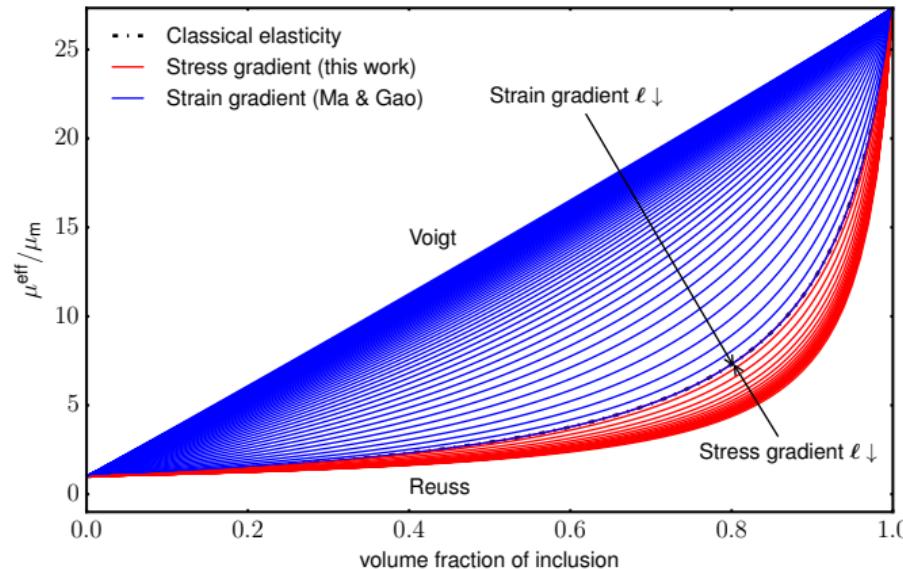
$$\mu_i = 27\mu_m, \nu_i = 0.4, \nu_m = 0.08, \ell_i = \ell_m = \ell$$



# Effect of material internal length (1)

Effective shear moduli (Mori Tanaka estimate)

$$\mu_i = 27\mu_m, \nu_i = 0.4, \nu_m = 0.08, \ell_i = \ell_m = \ell$$



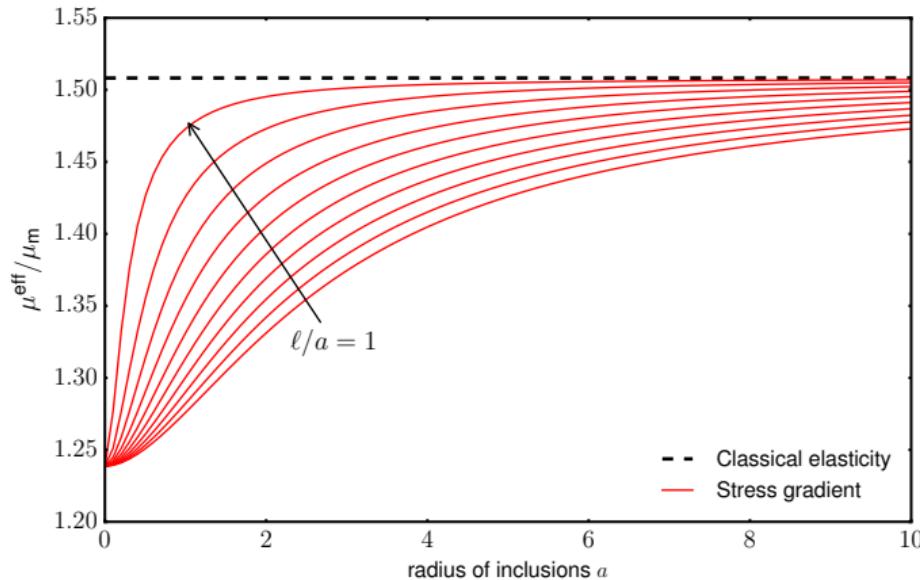
**Stress gradient is complementary to strain gradient elasticity!**

Ma, H.M, Gao, X.-L. Acta Mechanica, 225 (4-5), pp. 1075-1091, 2014

# Effect of material internal length (2)

Effective shear moduli:  $f = 20\%$

$$\mu_i = 27\mu_m, \nu_i = 0.4, \nu_m = 0.08, \ell_i = \ell_m = \ell$$



- Stress gradient elasticity: capture size effects.
- For  $a \gg \ell$ , stress gradient effects vanish as expected.



# Softening size effect

... has been reported elsewhere (molecular dynamics simulations)!

To cite some:

- Polyimide matrix "*reinforced*" by silica spherical nanoparticles with various surface treatment.

Odegard, G.M., Clancy, T.C., Gates, T.S. Polymer, 46, pp.553–562, 2005

- Polystyrene matrix "*reinforced*" by silica spherical nanoparticles.

Davydov, D., et al Soft Materials, 12, S142–S151, 2014

- etc



# Conclusion & Perspective

## Conclusion

- Solution to Eshelby's spherical inhomogeneity problem
- Mori Tanaka estimate for stress gradient materials
- Stress gradient elasticity differs from strain gradient elasticity
  - Strain gradient: stiffening size effect
  - Stress gradient: softening size effect

## Perspective

- Numerical implementation: FEM, FFT
- Physical interpretation of material internal length?

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**Thank you for your attention!**

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