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# Anisotropic thermal conductivity of natural Boom Clay

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31 **Abstract**

32 The thermal conductivity of host rocks is an important parameter in the design of deep geological  
33 disposal of heat-emitting radioactive waste. Due to bedding, heat transfer in sedimentary rocks is  
34 affected by their transversally isotropic structure. In this work, an experimental program is run to  
35 measure the thermal conductivities of Boom Clay along various orientations with respect to the  
36 bedding plane by using the needle thermal probe technique. Measurements were performed on  
37 specimens obtained from cores drilled from the HADES Underground Research Laboratory (URL) at  
38 Mol, Belgium, at a depth of 223 m. The thermal conductivities values obtained are in good agreement  
39 with those previously published, confirming the thermal anisotropy of the Boom Clay. Moreover, the  
40 observed changes in thermal conductivity with respect to the distance to the gallery provide further  
41 evidence on the extent of the Excavation Damaged Zone around the gallery.

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43 **Keywords:** Thermal conductivity; Boom Clay; thermal anisotropy; excavation damaged zone;  
44 laboratory test.

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56 **1 Introduction**

57 In the context of deep geological disposal of heat-emitting high activity radioactive waste, the thermal  
58 conductivity of the host geological formation (stiff clays, mudstones, granites, etc.) is an important

59 parameter in the design of the disposal. Moreover, the thermal transient phase that will be experienced  
60 by the system over hundreds to thousands of years after waste emplacement represents an important  
61 part of its long-term evolution (Yu et al., 2013). Due to a layered microstructure resulting from the  
62 initial deposition and further geological processes, stiff clays and claystones are known to  
63 preferentially conduct heat along the direction parallel to the bedding plane. Indeed, this anisotropy of  
64 thermal conductivity was observed in various stiff clays and claystones including the London clay, the  
65 Callovo-Oxfordian claystone (COx, East of France) and the Opalinus clay (Switzerland). In London  
66 clay, the thermal conductivity in the direction perpendicular to the bedding plane was found equal to  
67 0.83 W/(m.K) whereas that in the direction parallel to the bedding plane was equal to 1.19 W/(m.K)  
68 (Midttømme and Roaldset, 1999). The thermal conductivity of Opalinus Clay was investigated by  
69 Mügler et al. (2006). They reported that the values obtained by in-situ back analysis are 0.55 - 1.07  
70 W/(m.K) in the direction perpendicular to bedding and 1.84 - 1.90 W/(m.K) in the direction parallel to  
71 bedding, respectively. Buntebarth (2004) (in Jobmann and Polster, 2007) gave, from laboratory  
72 experiments, thermal conductivities of 0.75 W/(m.K) and 1.55 W/(m.K) for the directions  
73 perpendicular and parallel to bedding, respectively. The thermal conductivity in the direction  
74 perpendicular to the bedding plane of the COx claystone varies between 1.3 and 1.9 W/(m.K) whereas  
75 that in the direction parallel to the bedding plane varies between 1.9 and 2.7 W/(m.K) (ANDRA,  
76 2005).

77 Based on the values in the two directions, a degree of thermal conductivity anisotropy (or anisotropy  
78 effect)  $\eta$  can be defined, as follows (Popov et al., 1999; Pribnow et al., 2000; Davis et al., 2007):

$$\eta = \frac{\lambda_{//}}{\lambda_{\perp}} \quad (1)$$

79 From the values of thermal conductivity introduced above, a value of  $\eta = 1.43$  is determined for  
80 London clay. For Opalinus Clay and COx claystone,  $\eta$  can vary from 1.78 to 3.34 and from 1.42 to  
81 1.46, respectively.

82 In Boom Clay, the anisotropy of thermal conductivity has been inferred through the back analysis of a  
83 small scale in-situ heating experiment, ATLAS III, carried out in the Underground Research  
84 Laboratory (URL) HADES at a depth of 223 m (Chen et al., 2011). The measurements of temperature  
85 evolution at different distances from the heater were compared with the results of heat transfer

86 simulations. In those simulations, adopting values of thermal conductivities equal to 1.65 W/(m.K)  
87 and 1.31 W/(m.K) for the directions parallel and perpendicular to the bedding plane, respectively, led  
88 to good agreement with the measured temperatures. It is worth noting that, in some sedimentary  
89 rocks, the thermal conductivity in the direction parallel to the bedding plane is more than twice higher  
90 than that in the direction perpendicular to the bedding plane (Midttømme et al., 1996). After Schön  
91 (1996), the reasons for this anisotropy in thermal conductivity of sedimentary rocks are: (i) crystal  
92 anisotropy of the individual rock-forming minerals; (ii) intrinsic or structural anisotropy resulting from  
93 the mineral shapes and their textural arrangement within the rock; (iii) orientation and geometry of  
94 crack fractures and other defects. Point (ii) is particularly true in the case of clays and claystones  
95 because of the planar shape of clay platelets and the bedding orientation by long term consolidation,  
96 creep and diagenesis.

97

98 In addition to anisotropy, the presence of the Excavation Damage Zone (EDZ) around underground  
99 constructions can also influence the thermal conductivity. However, few studies have been devoted to  
100 this aspect.

101

102 Three methods are often used to measure the thermal conductivity of soils in the laboratory: i) the  
103 divided bar method, ii) the needle probe method (or line source method) and iii) optical scanning. The  
104 divided bar method is a steady state method in which a constant temperature gradient is imposed  
105 across the sample, resulting in a stable heat flow. This method involves heat transmission along a  
106 single direction only, and is considered to be accurate (Johansen, 1975; Farouki, 1981; Brigaud et al.,  
107 1990; Midttømme and Roaldset, 1999). It is also recommended to be used in measuring the thermal  
108 conductivity of rock samples (Beck, 1988; Ashworth, 1990). The needle probe method is a transient  
109 method in which a radial heat flow is produced within the specimen while measuring temperature  
110 changes over time. This method is based on the theory of axisymmetric heat diffusion from an infinite  
111 line source within an infinite surrounding medium. It is valid when the ratio between the length and  
112 the diameter of the needle is larger than 30:1 (Popov et al., 1999). The thermal conductivity can hence  
113 be back calculated from the temperature-time curve (Jessop, 1990). In the optical method (Popov,  
114 1983), a focused, mobile and continuously operated heat source is used to heat a sample while

115 monitoring temperature changes using infrared temperature sensors. The excess temperatures  
116 monitored on the sample are compared to that of a reference sample of known thermal conductivity,  
117 allowing the thermal conductivity to be determined. This method has been recommended to estimate  
118 the thermal anisotropy of rocks (Popov et al., 1999).

119

120 In this paper, the needle probe method was selected for its simplicity and standardisation. The thermal  
121 anisotropy of Boom Clay was investigated by adopting various orientations of the needle with respect  
122 to the bedding orientation of the samples. These experimental results were then compared with the  
123 theoretical results. The Boom Clay samples were extracted from a series of cores taken from a  
124 horizontal borehole drilled from a gallery of the HADES URL. The core was at 2.40 m to 22.3 m  
125 distance to the gallery axis (HADES borehole 2012-2 / Connecting Gallery / Ring 66-67W) and the  
126 specimens were extracted from the core at various distances ranging from 2.5 to 20.8 m to the gallery  
127 axis.

128

## 129 **2 Background**

### 130 **2.1 Anisotropy of thermal conductivity**

131 Heat flow by conduction along one dimension is governed by Fourier's law:

$$q = -\lambda \frac{dT}{dx} \quad (2)$$

132 where  $q$  is the heat flux density ( $\text{W}/\text{m}^2$ ),  $\lambda$  is the thermal conductivity ( $\text{W}/(\text{m}\cdot\text{K})$ ) and  $dT/dx$  is the  
133 temperature gradient along the  $x$  direction.

134 In an anisotropic material, the apparent thermal conductivity  $\lambda$  measured on an anisotropic sample  
135 around a line-source is related to the principal components of the thermal conductivity tensor (Grubbe  
136 et al., 1983; Popov et al., 1999), as follows:

$$\lambda = \sqrt{\lambda_A \lambda_B \cos^2(\gamma) + \lambda_A \lambda_C \cos^2(\beta) + \lambda_B \lambda_C \cos^2(\alpha)} \quad (3)$$

137 where,  $\lambda_A$ ,  $\lambda_B$  and  $\lambda_C$  are the three principal components of the thermal conductivity tensor;  $\alpha$ ,  $\beta$  and  $\gamma$   
138 are the angles between the line-source axis and the principal directions of thermal conductivity tensor

139 A, B and C, respectively (Fig. 1). Knowing the angles  $\alpha$ ,  $\beta$  and  $\gamma$  in equation (3), the apparent thermal  
 140 conductivity  $\lambda$  can be determined through three measurements.

141 Due to the stratification and bedding, many sedimentary rocks and clays are transversely isotropic,  
 142 leading to the following relations:  $\lambda_A = \lambda_{\perp}$  (thermal conductivity in the direction perpendicular to the  
 143 bedding plane) and  $\lambda_B = \lambda_C = \lambda_{//}$  (thermal conductivity in the direction parallel to the bedding plane). If  
 144 the axis of the emitting needle probe is perpendicular to the bedding plane (Fig. 1a),  $\alpha = 0^\circ$  and  $\beta = \gamma$   
 145  $= 90^\circ$ . Hence:

$$\lambda_0 = \sqrt{\lambda_B \lambda_C \cos^2(0^\circ)} = \lambda_{//} \quad (4)$$

146 When the needle is parallel to the bedding plane (Fig. 1b),  $\alpha = \gamma = 90^\circ$ ,  $\beta = 0^\circ$  and  $\lambda$  represents  $\lambda_{90}$ :

$$\lambda_{90} = \sqrt{\lambda_A \lambda_C \cos^2(0^\circ)} = \sqrt{\lambda_{\perp} \lambda_{//}} \quad (5)$$

147 From (4) and (5):

$$\lambda_{\perp} = \frac{(\lambda_{90})^2}{\lambda_0} \quad (6)$$

148 Equation (6) has been used by several authors (Penner, 1963; Munroe and Sass, 1987; Popov et al.,  
 149 1999; Pribnow et al., 2000; Gong, 2005; Davis et al., 2007; Popov et al., 2012; Riche and Schneebeil,  
 150 2012) to determine the value of thermal conductivity in the direction perpendicular to bedding  $\lambda_{\perp}$   
 151 based on the measurements of  $\lambda_{90}$  and  $\lambda_0$  in different materials (clay sediments, igneous rocks, snow,  
 152 etc.).

153

154 In general, when the line source axis forms an angle  $\theta$  with the normal to the bedding (Fig. 1c), an  
 155 apparent thermal conductivity can be determined by:

$$\lambda_{\theta} = \sqrt{\lambda_{\perp} \lambda_{//} \sin^2(\theta) + (\lambda_{//})^2 \cos^2(\theta)} \quad (7)$$

156 Thus,

$$\lambda_{\theta} = \sqrt{(\lambda_0)^2 \cos^2(\theta) + (\lambda_{90})^2 \sin^2(\theta)} \quad (8)$$

157 Equation (8) was firstly proposed by Pribnow (cited by Davis et al., 2007). This function was used to  
 158 compare the experimental results with the changes in probe orientation. The data of Davis et al. (2007)  
 159 agree reasonably well with equation (8).

160 To calculate the value for  $\theta = 45^\circ$ , substituting equation (6) into equation (8) yields:

$$\lambda_{45} = \sqrt{\frac{(\lambda_0)^2 + (\lambda_{90})^2}{2}} \quad (9)$$

161

## 162 **2.2 Thermal conductivity at saturated state**

163 Various authors stated that the thermal conductivity of clays depends on several factors such as the  
164 composition (solid, water and gas phases), the nature of the dominant minerals, the density/porosity,  
165 the temperature, etc. (Farouki, 1986; Clauser and Huenges, 1995; Midttømme and Roaldset, 1999;  
166 Tang et al., 2008). In this study, the effects of the slight changes in degree of saturation ( $S_r$ ) and  
167 density of the investigated samples were taken into account based on the Johansen's method (Farouki,  
168 1986). According to Johansen, the thermal conductivity of an unsaturated soil is a function of its  
169 thermal conductivity at dry and saturated states at the same dry density. To establish this function,  
170 Johansen (1975) introduced a normalized thermal conductivity, namely Kersten's number ( $K_e$ ):

$$K_e = (\lambda - \lambda_{dry}) / (\lambda_{sat} - \lambda_{dry}) \quad (10)$$

171 where  $\lambda_{sat}$  is the thermal conductivity at saturated state,  $\lambda$  is the thermal conductivity at intermediate  
172 degree of saturation,  $\lambda_{dry}$  is the thermal conductivity at dry state

173 Hence, one can deduce the saturated thermal conductivity value from the thermal conductivity  
174 measurement conducted on non-saturated samples, according to the following relationship:

$$\lambda_{sat} = \frac{(\lambda - \lambda_{dry})}{K_e} + \lambda_{dry} \quad (11)$$

175 In fine-grained unfrozen soils, Johansen proposes the following relationships for  $K_e$  and  $\lambda_{dry}$ :

$$K_e \cong \log S_r + 1.0 \quad (12)$$

176

$$\lambda_{dry} = \frac{0.135\rho_d + 64.7}{2700 - 0.947\rho_d} \pm 20\% \text{ (W / (m.K))} \quad (13)$$

177 where  $\rho_d$  is the dry density in  $\text{kg/m}^3$ .



## 178 **3 Material and methods**

### 179 **3.1 The Boom Clay**

180 In Belgium, researches on geological radioactive waste disposal in clay formation were initiated by  
181 SCK•CEN in 1974. The first Underground Research Laboratory (URL) HADES was then excavated  
182 in Boom Clay formation at a depth of 223 m during the early Eighties at a site close to the city of Mol  
183 and has been progressively extended since. The Boom Clay was chosen as a potential host rock for  
184 radioactive waste disposal due to its very low permeability (its hydraulic conductivity around  $2 \cdot 10^{-12}$   
185 m/s and  $5 \cdot 10^{-12}$  m/s in the direction perpendicular and parallel to the bedding, respectively), its  
186 capacity to retard the migration of many radionuclides by sorption, its high plasticity, and its capacity  
187 of self-sealing after physical disturbances.

188

189 Located at 190 m - 290 m below ground level at Mol (ONDRAF/NIRAS, 2001), Boom Clay was  
190 deposited during the Tertiary Era about 30 millions years ago. The Boom Clay layer is almost  
191 horizontal with a slight 1-2% north-east dip. It is located between water-bearing sand layers  
192 (ONDRAF/NIRAS, 2001).

193

194 In order to investigate both the anisotropy in thermal conductivity of Boom Clay and the possible  
195 influence of the excavation damaged zone (EDZ) on it, nine samples were taken at various distances  
196 from the gallery (4.0 m in diameter, 0.4 m in liner thickness) from the core (100 mm in diameter)  
197 taken from a borehole (reference number: R66-67/2012) drilled horizontally till approximately 22 m in  
198 length, in July 2012. Once drilled, the core was immediately sealed under vacuum in aluminium foils  
199 to minimize drying effects. Table 1 summarizes the physical properties of the nine samples. The  
200 distance to the gallery axis  $r$  varies from 2.5 m to 20.8 m. The water content of the samples ( $w$ )  
201 slightly changes from 22.6% to 24%, which is in the range of the in-situ measurements (from 22% to  
202 27%). The densities are comparable ( $1630$ - $1640$  kg/m<sup>3</sup>) except for the sample that was the closest to  
203 the gallery (TH6,  $r = 2.9$  m,  $\rho_d = 1.61$  Mg/m<sup>3</sup>). A suction measurement was made on sample TH11 ( $r$   
204 = 9.60 m) using a chilled mirror hygrometer (WP4, Decagon Device), and a value of 2.8 MPa was

205 obtained, in good agreement with the suction value reported in Delage et al. (2007) from a sample at  
206 the same depth.

207

### 208 **3.2 Thermal conductivity measurements**

209 The apparatus used to measure the thermal conductivity is a commercial handheld device named KD2  
210 Pro Thermal Properties Analyzer (Decagon Devices, Inc.). The kit consists of a controller and 3  
211 separated sensors (small single needle, large single needle, dual needle) that can be inserted into the  
212 tested medium. The small single needle (60 mm in length, 1.3 mm in diameter) (Fig. 2b) was used to  
213 measure the thermal conductivity of Boom Clay. The accuracy of the thermal conductivity  
214 measurement using this needle is  $\pm 5\%$  from 0.2 W/(m.K) - 2 W/(m.K).

215

216 Cylindrical samples were trimmed from cores (100 mm in diameter and 60mm - 90 mm in height).  
217 The bedding orientation that could be identified from direct visual observation was marked. The  
218 samples were then slightly confined by means of an adhesive tape so as to avoid further crack  
219 propagation and any perturbation.

220

221 Three holes were prepared in each sample by drilled in each sample using a drilling-machine (Fig. 2a)  
222 equipped with a thin steel drill (1.3 mm in diameter, 65 mm in effective length). In order to ensure a  
223 good thermal contact between specimen and probe, the needle probe was coated with a thin layer of  
224 thermal grease (high-density polysynthetic silver thermal compound by Arctic Silver) prior to its  
225 insertion into the drilled hole (Fig. 2b), as recommended by the ASTM standard D5334-08 (2008). For  
226 a better precision, it was decided to run 5 successive measurements at intervals of 15 minutes.

227

228 The measured thermal conductivity values were denoted  $\lambda_0$ ,  $\lambda_{45}$  and  $\lambda_{90}$ , defined by the value of the  
229 angle  $\theta$  between the axis of the hole and the direction normal to the bedding (see Fig. 1 and Fig. 3). As  
230 mentioned previously, heat transfer in the case of  $\theta = 0^\circ$  is parallel to the bedding (Fig. 1a), and the  $\lambda_0$   
231 value measured by the needle device is equal to the thermal conductivity in the direction parallel to the  
232 bedding ( $\lambda_{//}$ ). In the two other cases, the measured values depend on the thermal conductivities in the

233 directions parallel and perpendicular to the bedding. The thermal conductivity in the direction  
234 perpendicular to the bedding ( $\lambda_{\perp}$ ) needs to be back calculated, as seen in the previous section.

235

## 236 **4 Experimental results**

### 237 **4.1 Anisotropy of thermal conductivity**

238 Since the degrees of saturation of the nine specimens are slightly lower than 100% (see Table 1), the  
239 thermal conductivities at saturated state were first calculated using equation (11). As seen in Table 2 in  
240 which the initial ( $\lambda_{i/0}$ ) and corrected  $\lambda_{i/}$  values are presented, the corrections made for saturation are  
241 small with a relative variation ( $\Delta\lambda_{i/} / \lambda_{i/0}$ ) included between 0.64% and 2.04%. The values of thermal  
242 conductivity in the direction perpendicular to the bedding at saturated state  $\lambda_{\perp}$  were afterwards  
243 determined using equation (6) based on the value of  $\lambda_{90}$  determined from a test with the needle parallel  
244 to the bedding (Fig. 3). The thermal conductivity anisotropy ratio  $\eta$  was then deduced from equation

245 **Erreur ! Source du renvoi introuvable..**

246

### 247 **4.2 Influence of EDZ on thermal conductivity**

248 The changes in thermal conductivity along the three directions ( $\lambda_0$ ,  $\lambda_{45}$ ,  $\lambda_{90}$ , Fig. 3) with respect to the  
249 distance to the gallery axis  $r$  are shown in Fig. 4. The gallery wall is also represented in this figure.  
250 The vertical bars indicate the range of the 5 measurements performed on each sample. The calculated  
251 values of  $\lambda_{45}$  (from  $\lambda_0$  and  $\lambda_{90}$  using equation (9)) are also plotted for comparison with the test data  
252 directly obtained using the needle probe inclined at  $45^\circ$  with respect to the bedding. Excellent  
253 agreement was observed, confirming: (i) 2D anisotropy model (presented in the part 2.1), (ii)  
254 correspondence of principal axes of thermal conductivity to bedding plane orientation shown in Figure  
255 1.

256 Fig. 4 shows that all the measurements start from a low value in the zone close to the gallery wall  
257 (around 1.3 W/(m.K) for  $\lambda_0 = \lambda_{i/}$  at  $r = 2.5$  m). The conductivity values increase with distance to reach  
258 a maximum value at around 6.4 m from the gallery axis (1.6 W/(m.K) for  $\lambda_{i/}$ ). A slight decrease ( $\lambda_{i/}$ ) or  
259 a more significant one ( $\lambda_{\perp}$ ) is observed for samples taken at greater distances from the gallery (up to

260 20.8 m). The average value of 1.6 W/(m.K) for  $\lambda_{//}$  observed at larger distances is in good agreement  
261 with the value of 1.65 W/(m.K) obtained from the back calculations carried out within the ATLAS III  
262 project (Chen et al., 2011; Yu et al., 2011).

263

264 These results also confirm that the thermal conductivity in the direction parallel to the bedding is  
265 always higher than that in the direction perpendicular to the bedding. The values of  $\lambda_{//}$  vary between  
266 1.34 - 1.61 W/(m.K) whereas those of  $\lambda_{\perp}$  vary between 0.82 – 1.06 W/(m.K) (Fig. 4). This can also be  
267 observed in Fig. 5 that presents the changes in anisotropy ratios  $\eta$  versus the distance  $r$  to the gallery  
268 axis. The values of  $\eta$  change between 1.5 and 1.8 with no significant effect of the distance to the  
269 gallery axis. Note that the value of  $\lambda_{\perp}$  obtained in this study is smaller than that obtained by back  
270 calculations (1.31 W/(m.K)) by Chen et al. (2011). This difference may be explained by the fact that  
271  $\lambda_{\perp}$  is much more dependent on confinement (that strongly affects the contact between parallel clay  
272 particles) than  $\lambda_{//}$ . Further studies on the effect of confinement on the anisotropic thermal conductivity  
273 are needed to confirm this point.

274

## 275 **5 Discussion**

276 It is now well recognized that an Excavation Damaged Zone (EDZ) characterized by a fracture  
277 network including shear and tension fractures along with a herringbone pattern of fractures develops  
278 during excavation in clays and claystones (Mertens et al., 2004; Bastiaens and Mertens, 2005; Davies  
279 and Bernier, 2005; Tsang et al., 2005; Bernier et al., 2007; Tsang et al., 2012; Armand et al., 2013).  
280 The extent of this zone depends on various parameters such as the nature of the media (soft clay, stiff  
281 clay or claystone), its mechanical properties, the excavation technique, the state of stress around the  
282 gallery and the bedding orientation. Around the Connecting Gallery of the URL HADES at Mol, an  
283 EDZ characterized by a herringbone fracture pattern has been observed (Bastiaens and Mertens, 2005;  
284 Bernier et al., 2007) with open fractures extending to about 1 m from the gallery wall. There were  
285 indications that the extent in the horizontal direction was somewhat larger than in the vertical  
286 direction.

287

288 The thermal conductivity measurements carried out in this study on samples extracted from a  
289 horizontal borehole at various distances from the gallery axis evidenced changes that can be related to  
290 the EDZ, given that discontinuities are suspected to affect heat transfer across these. In this regard, the  
291 thermal conductivity changes in the direction parallel to the bedding ( $\lambda_{//}$ ) seems to be the more  
292 significant parameter to be considered since the borehole was horizontal with a sub-vertical orientation  
293 of cracks in this area. Indeed, inspection of Fig. 4 shows that parameter  $\lambda_{//}$  starts from small values to  
294 afterwards increase with the distance to the gallery (until a distance  $r$  of 4.0 m from the gallery axis,  
295 corresponding to about 1.6 m from the outside wall). Beyond this distance, the horizontal thermal  
296 conductivity remains about constant, around a value of 1.6 W/(m.K), in good accordance with the  
297 back analysis of the in-situ heating test. Based on the thermal conductivity measurements, it is  
298 deduced that the EDZ extension in the horizontal direction is about 1.6 m from the outside of gallery's  
299 wall, a value in consistence with in situ observation.

300

301 The data presented here were obtained from the laboratory measurements carried out on samples  
302 extracted from a horizontal core and under zero confining stress. As a result, there would be some  
303 possibility of cracks' opening within the samples due to stress release. Thereby, the effects of cracks  
304 on thermal fluxes observed in Fig. 4 could be enhanced by the stress release. Thus, the question arises  
305 as to whether the changes in thermal conductivity with respect to the distance to the gallery really  
306 occur in-situ. Actually, clays are known to exhibit self-sealing properties with respect to water  
307 transfer. This self-sealing behaviour, interpreted as the recovery of a good contact between the two  
308 faces of discontinuities, could have comparable consequence on heat transfer as well. In other words,  
309 self-sealing could be extended from fluid transfer to heat transfer. Such a hypothesis should obviously  
310 be further investigated by thermal conductivity measurements in the laboratory, under confining  
311 conditions and/or running detailed in-situ measurement at various distances from the gallery  
312 completed by thermal back-analysis of in-situ thermal tests. Meanwhile, the changes in thermal  
313 conductivity carried out here on laboratory samples provide a complementary identification of the  
314 extent of the EDZ along a horizontal direction around the gallery excavated in Boom Clay.

315

## 316 **6 Conclusion**

317 An experimental study using the needle thermal probe technique was conducted for investigating the  
318 thermal conductivity anisotropy of natural Boom Clay. The investigation was carried out on samples  
319 extracted from a series of cores (from a single borehole) taken from the Underground Research  
320 Laboratory at Mol in Belgium, at a depth of 223 m. Thermal conductivity was measured on specimens  
321 sampled at various distances to the gallery axis, from 2.5 to 20.8 m. Measurements were conducted  
322 along three directions: parallel, perpendicular and at an angle of 45° with respect to the bedding plane.  
323 A significant thermal anisotropy was evidenced and data confirmed that the highest conductivity was  
324 in the direction parallel to bedding and that the smallest one was in the direction perpendicular to  
325 bedding, the one at 45° being logically in between these two values. It is worth noting that the  
326 conductivity values found in this laboratory study in the direction parallel to the bedding was close to  
327 that back-calculated from the in-situ ATLAS experiments (Chen et al., 2011).

328 The effect of an excavation damaged zone (EDZ) was also evidenced: the thermal conductivity in the  
329 three directions increased with the distance to the gallery. Based on the experimental data, an EDZ  
330 extent of about 1.6 m in the horizontal direction was identified, a value consistent with the in situ  
331 observation. Finally, the thermal anisotropy did not appear to be significantly affected by the  
332 excavation damage, with no significant effect of the distance to the gallery on the thermal anisotropy  
333 ratio that was comprised between 1.48 and 1.74.

334

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339

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459 **List of Tables**

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462 Table 2: Initial and corrected  $\lambda_{//}$  values ( $\lambda_{//0}$ : thermal conductivity measured on non-saturated samples,  
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477 Table 1: Properties of natural Boom Clay samples taken at various distances  $r$  to gallery axis ( $\rho_d$  : dry  
478 density,  $w$ : water content,  $e$ : void ratio,  $S_r$ : degree of saturation)

Test	Distance $r$ (m)	$\rho_d$ (kg/m <sup>3</sup> )	$w$ (%)	$e$	$S_r$ (%)
TH6	2.5	1610	23.98	0.65	97.9
TH7	2.6	1640	23.05	0.63	98.0
TH8	2.7	1640	23.05	0.63	98.0
TH14	3.4	1630	23.51	0.64	98.4
TH13	3.8	1630	23.02	0.63	98.0
TH12	6.0	1630	22.84	0.64	95.2
TH11	9.2	1640	22.63	0.63	96.3
TH10	16.0	1640	22.61	0.63	96.2
TH9	20.8	1630	23.48	0.64	98.4

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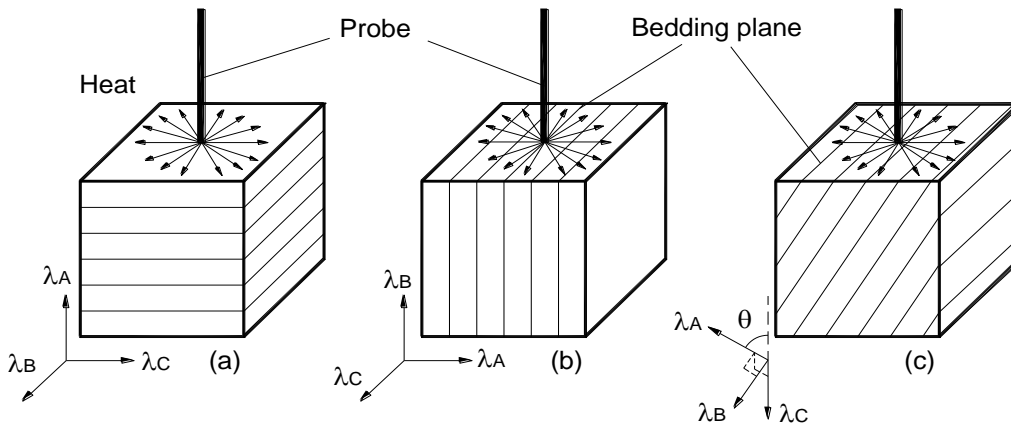
Tests	Distance $r$ (m)	$S_r$	$\lambda_{//0}$ (W/(m.K))	Corrected $\lambda_{//}$ (W/(m.K))	$\Delta\lambda_{//} / \lambda_{//(\text{measured})}$ (%)
TH6	2.5	97.9	1.33	1.34	0.85
TH7	2.6	98.0	1.38	1.39	0.80
TH8	2.7	98.0	1.41	1.42	0.80
TH14	3.4	98.4	1.45	1.46	0.64
TH13	3.8	98.0	1.54	1.55	0.81
TH12	6.0	95.2	1.56	1.59	2.04
TH11	9.2	96.3	1.58	1.61	1.55
TH10	16.0	96.2	1.49	1.51	1.57
TH9	20.8	98.4	1.52	1.53	0.67

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492 A, B and C: main (orthogonal) axes of thermal conductivity (A is perpendicular to the bedding plane;

493 B and C are parallel to the bedding plane).

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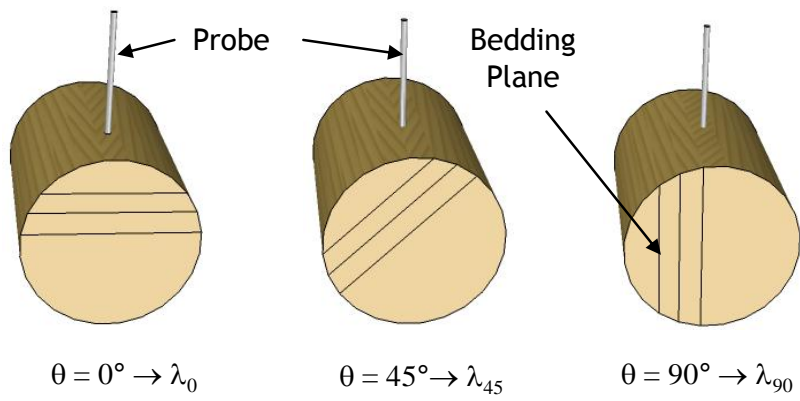
(a)

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498 probe into the specimen with marks of the bedding plane.

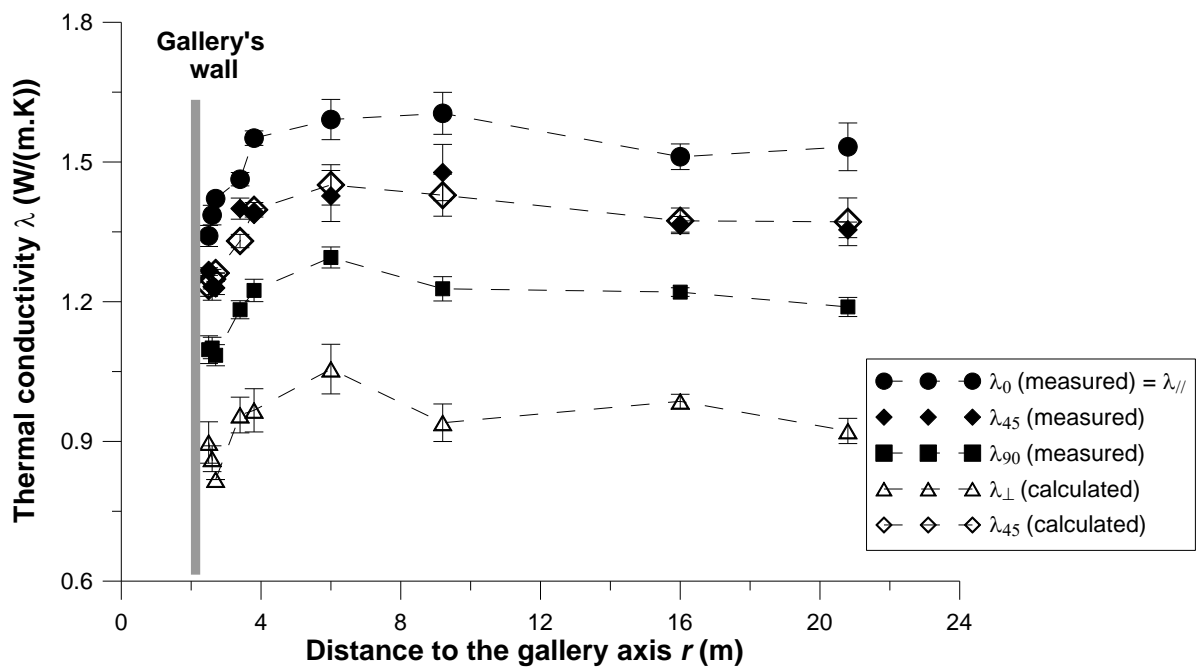
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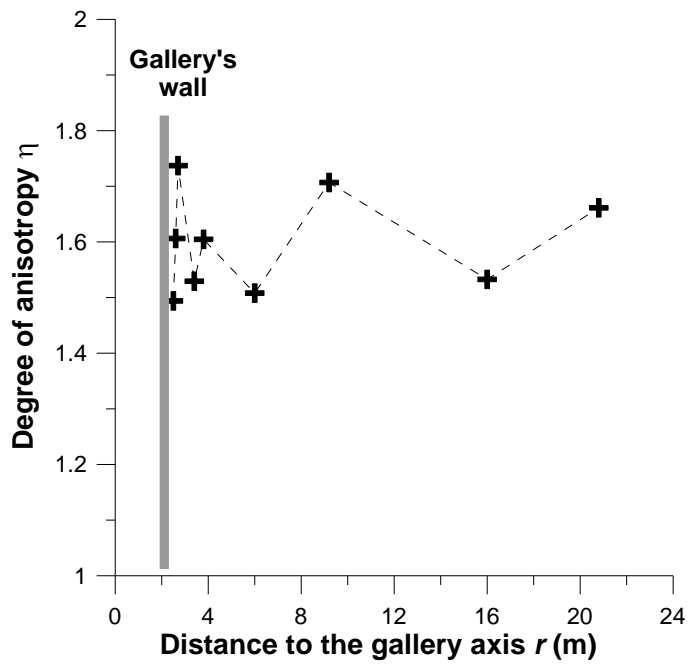
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504 Fig. 4: Thermal conductivity versus distance  $r$  to the axis of the gallery.

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509 Fig. 5: Degree of thermal conductivity anisotropy versus distance  $r$  to the axis of the gallery.

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